

Fundamentals of Signal Enhancement and Array Signal Processing Solution Manual

Lidor Malul 318628005

9 Differential Beamforming

9.2

Show that the coefficients of the N th-order hypercardioid are given by

$$\mathbf{a}_{N,\max} = \frac{\mathbf{H}_N^{-1}\mathbf{1}}{\mathbf{1}^T \mathbf{H}_N^{-1}\mathbf{1}}.$$

Solution:

First we can notice that the rank of the matrix $\mathbf{1}\mathbf{1}^T$ is 1. So , the rank of the matrix $\mathbf{H}_N^{-1}\mathbf{1}\mathbf{1}^T$ is 1 or 0. Therefor, for the non zero eigenvalue , the eigenvector is the maximum.

lets show that \mathbf{a}_N is eigenvector for non zero eigenvalue:

$$(\mathbf{H}_N^{-1}\mathbf{1}\mathbf{1}^T) \mathbf{a}_N = (\mathbf{H}_N^{-1}\mathbf{1}\mathbf{1}^T) \frac{\mathbf{H}_N^{-1}\mathbf{1}}{\mathbf{1}^T \mathbf{H}_N^{-1}\mathbf{1}} = \frac{\mathbf{H}_N^{-1}\mathbf{1}}{\mathbf{1}^T \mathbf{H}_N^{-1}\mathbf{1}} \mathbf{1} \mathbf{H}_N^{-1}\mathbf{1} = \mathbf{a}_N (\mathbf{1} \mathbf{H}_N^{-1}\mathbf{1}) = \mathbf{a}_N \cdot \lambda$$

which $\lambda \triangleq \mathbf{1} \mathbf{H}_N^{-1}\mathbf{1}$ scalar , non zero eigenvalue of $\mathbf{H}_N^{-1}\mathbf{1}\mathbf{1}^T$

\mathbf{a}_N is the eigenvector corresponding to the maximum eigenvalue of the matrix.

■

9.3

Using the definition of the frequency-independent FBR of a theoretical N th-order DSA (??), show that

$$\mathcal{F}(\mathbf{a}_N) = \frac{\mathbf{a}_N^T \mathbf{H}_N'' \mathbf{a}_N}{\mathbf{a}_N^T \mathbf{H}_N' \mathbf{a}_N},$$

where \mathbf{H}'_N and \mathbf{H}''_N are Hankel matrices.

Solution:

We know that the FBR define as:

$$F(a_N) = \frac{\int_0^{\frac{\pi}{2}} B^2(a_N, \cos \theta) \sin \theta d\theta}{\int_{\frac{\pi}{2}}^{\pi} B^2(a_N, \cos \theta) \sin \theta d\theta}$$

and B define as:

$$B(a_N, \cos \theta) = \sum_{n=0}^{n=N} a_{N,n} \cos^n \theta$$

now we substitute B in FBR definition:

$$F(a_N) = \frac{\int_0^{\frac{\pi}{2}} \sum_{n=0}^{n=N} a_{N,n} \cos^n \theta \sum_{k=0}^{k=N} a_{N,k} \cos^k \theta \sin \theta d\theta}{\int_{\frac{\pi}{2}}^{\pi} \sum_{n=0}^{n=N} a_{N,n} \cos^n \theta \sum_{k=0}^{k=N} a_{N,k} \cos^k \theta \sin \theta d\theta} = \frac{\sum_{k=0}^{k=N} \sum_{n=0}^{n=N} a_{N,n} a_{N,k} \int_0^{\frac{\pi}{2}} \cos^n \theta \cos^k \theta \sin \theta d\theta}{\sum_{k=0}^{k=N} \sum_{n=0}^{n=N} a_{N,n} a_{N,k} \int_{\frac{\pi}{2}}^{\pi} \cos^n \theta \cos^k \theta \sin \theta d\theta} = \otimes$$

using the following solutions:

$$\int_0^{\frac{\pi}{2}} \cos^i \theta \cos^j \theta \sin \theta d\theta = \frac{1}{1+i+j} = [H''_N]_{ij}$$

$$\int_{\frac{\pi}{2}}^{\pi} \cos^i \theta \cos^j \theta \sin \theta d\theta = \frac{(-1)^{i+j}}{1+i+j} = [H'_N]_{ij}$$

finally:

$$\otimes = \frac{\sum_{k=0}^{N-1} \sum_{n=0}^{N-1} a_{N,n} a_{N,k} [H''_N]_{nk}}{\sum_{k=0}^{N-1} \sum_{n=0}^{N-1} a_{N,n} a_{N,k} [H'_N]_{nk}} = \frac{a_N^T H''_N a_N}{a_N^T H'_N a_N}$$

where H''_N and H'_N are two Hankel matrices.

■

9.5

Show that the directivity pattern of the first-order hypercardioid can be expressed as

$$B_{1,\text{Hd}}(\cos \theta) = \frac{1}{4} + \frac{3}{4} \cos \theta.$$

Solution:

We know the definition of B:

$$B_{N,\text{Hd}}(\cos \theta) = \frac{1^T H^{-1}_N p(\cos \theta)}{1^T H^{-1}_N 1}$$

and for N=1:

$$p(\cos \theta) = [1 \quad \cos \theta]^T$$

$$1^T = [1 \quad 1]$$

$$1 = [1 \quad 1]^T$$

$$H_1 = \begin{pmatrix} 1 & 0 \\ 0 & \frac{1}{3} \end{pmatrix} \rightarrow H_1^{-1} = \begin{pmatrix} 1 & 0 \\ 0 & 3 \end{pmatrix}$$

substituting:

$$B_{N,\text{Hd}}(\cos \theta) = \frac{[1 \quad 1] \begin{pmatrix} 1 & 0 \\ 0 & 3 \end{pmatrix} [1 \quad \cos \theta]^T}{[1 \quad 1] \begin{pmatrix} 1 & 0 \\ 0 & 3 \end{pmatrix} [1 \quad 1]^T} = \frac{1 + 3 \cos \theta}{4} = \frac{1}{4} + \frac{3 \cos \theta}{4}$$

■

9.6

Show that the directivity pattern of the first-order supercardioid can be expressed as

$$B_{1,\text{Sd}}(\cos \theta) = \frac{\sqrt{3}-1}{2} + \frac{3-\sqrt{3}}{2} \cos \theta.$$

Solution:

The beampattern of the Nth-order supercardioid is

$$B_{N,\text{Sd}}(\cos \theta) = \frac{a'_{N,\text{max}}^T p(\cos \theta)}{a'_{N,\text{max}}^T p(1)}$$

when $a_{N,\max}^{'T}$ is the eigenvector corresponding to the maximum eigenvalue of $H_N'^{-1}H_1''$

for N=1:

$$H_1' = \begin{pmatrix} 1 & -\frac{1}{2} \\ -\frac{1}{2} & \frac{1}{3} \end{pmatrix} \rightarrow H_1'^{-1} = \begin{pmatrix} 4 & 6 \\ 6 & 12 \end{pmatrix}$$

$$H_1'' = \begin{pmatrix} 1 & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{3} \end{pmatrix}$$

$$H_N'^{-1}H_1'' = \begin{pmatrix} 4 & 6 \\ 6 & 12 \end{pmatrix} \begin{pmatrix} 1 & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{3} \end{pmatrix} = \begin{pmatrix} 7 & 4 \\ 12 & 7 \end{pmatrix}$$

the max eigenvalue of the matrix $\begin{pmatrix} 7 & 4 \\ 12 & 7 \end{pmatrix}$ is $\lambda_{\max} = 7 + 4\sqrt{3}$ the eigenvector for the max eigenvalue is : $\begin{pmatrix} \sqrt{3}-1 \\ 3-\sqrt{3} \end{pmatrix}$
So:

$$a_{N,\max}' = \begin{pmatrix} \sqrt{3}-1 \\ 3-\sqrt{3} \end{pmatrix}$$

And finally:

$$B_{1,Sd}(\cos \theta) = \frac{(\sqrt{3}-1 \quad 3-\sqrt{3})(1 \quad \cos \theta)^T}{\sqrt{3}-1+3-\sqrt{3}} = \frac{\sqrt{3}-1}{2} + \frac{3-\sqrt{3}}{2} \cos \theta$$

■

9.7

Show that the directivity pattern of the second-order hypercardioid can be expressed as

$$B_{2,Hd}(\cos \theta) = -\frac{1}{6} + \frac{1}{3} \cos \theta + \frac{5}{6} \cos^2 \theta.$$

Solution:

We know the definition of B:

$$B_{N,Hd}(\cos \theta) = \frac{1^T H^{-1} N p(\cos \theta)}{1^T H^{-1} N 1}$$

and for N=2:

$$p(\cos \theta) = [1 \quad \cos \theta \quad \cos^2 \theta]^T$$

$$1^T = [1 \quad 1 \quad 1]$$

$$1 = [1 \quad 1 \quad 1]^T$$

$$H_1 = \begin{pmatrix} 1 & 0 & \frac{1}{3} \\ 0 & \frac{1}{3} & 0 \\ \frac{1}{3} & 0 & \frac{1}{5} \end{pmatrix} \rightarrow H_1^{-1} = \begin{pmatrix} \frac{9}{4} & 0 & -\frac{15}{4} \\ 0 & \frac{12}{4} & 0 \\ -\frac{15}{4} & 0 & \frac{45}{4} \end{pmatrix}$$

and now:

$$B_{2,Hd} = \frac{[1 \quad 1 \quad 1] \begin{pmatrix} \frac{9}{4} & 0 & -\frac{15}{4} \\ 0 & \frac{12}{4} & 0 \\ -\frac{15}{4} & 0 & \frac{45}{4} \end{pmatrix} [1 \quad \cos \theta \quad \cos^2 \theta]^T}{[1 \quad 1 \quad 1] \begin{pmatrix} \frac{9}{4} & 0 & -\frac{15}{4} \\ 0 & \frac{12}{4} & 0 \\ -\frac{15}{4} & 0 & \frac{45}{4} \end{pmatrix} [1 \quad 1 \quad 1]^T} = \frac{[-\frac{6}{4} \quad \frac{12}{3} \quad \frac{30}{4}] [1 \quad \cos \theta \quad \cos^2 \theta]^T}{\frac{36}{4}} =$$

$$= -\frac{1}{6} + \frac{1}{3} \cos \theta + \frac{5}{6} \cos^2 \theta$$

■

9.8

Show that the directivity pattern of the second-order supercardioid can be expressed as

$$B_{2,Sd}(\cos \theta) = \frac{1}{2(3 + \sqrt{7})} + \frac{\sqrt{7}}{3 + \sqrt{7}} \cos \theta + \frac{5}{2(3 + \sqrt{7})} \cos^2 \theta.$$

Solution:

The beampattern of the Nth-order supercardioid is

$$B_{N,Sd}(\cos \theta) = \frac{a'_{N,\max}^T p(\cos \theta)}{a'_{N,\max}^T p(1)}$$

when $a'_{N,\max}$ is the eigenvector corresponding to the maximum eigenvalue of $H_N'^{-1} H_1''$

for N=2:

$$\begin{aligned} H_2' &= \begin{pmatrix} 1 & -\frac{1}{2} & \frac{1}{3} \\ -\frac{1}{2} & \frac{1}{3} & -\frac{1}{4} \\ \frac{1}{3} & -\frac{1}{4} & \frac{1}{5} \end{pmatrix} \rightarrow H_2'^{-1} = \begin{pmatrix} 9 & 36 & 30 \\ 36 & 192 & 180 \\ 30 & 180 & 180 \end{pmatrix} \\ H_2'' &= \begin{pmatrix} 1 & \frac{1}{2} & \frac{1}{3} \\ \frac{1}{2} & \frac{1}{3} & \frac{1}{4} \\ \frac{1}{3} & \frac{1}{4} & \frac{1}{5} \end{pmatrix} \\ H_2'^{-1} H_2'' &= \begin{pmatrix} 9 & 36 & 30 \\ 36 & 192 & 180 \\ 30 & 180 & 180 \end{pmatrix} \begin{pmatrix} 1 & \frac{1}{2} & \frac{1}{3} \\ \frac{1}{2} & \frac{1}{3} & \frac{1}{4} \\ \frac{1}{3} & \frac{1}{4} & \frac{1}{5} \end{pmatrix} = \begin{pmatrix} 37 & 24 & 18 \\ 192 & 127 & 96 \\ 180 & 120 & 91 \end{pmatrix} \end{aligned}$$

the max eigenvalue of the matrix $H_2'^{-1} H_2''$ is $\lambda_{\max} = 127 + 48\sqrt{7}$ the eigenvector for the max eigenvalue is : $\begin{pmatrix} 1 \\ 2\sqrt{7} \\ 5 \end{pmatrix}$

So:

$$a'_{2,\max} = \begin{pmatrix} 1 \\ 2\sqrt{7} \\ 5 \end{pmatrix}$$

And finally:

$$B_{2,Sd}(\cos \theta) = \frac{\begin{pmatrix} 1 \\ 2\sqrt{7} \\ 5 \end{pmatrix}^T (1 \ cos \theta \ cos^2 \theta)^T}{1 + 2\sqrt{7} + 5} = \frac{1}{2(3 + \sqrt{7})} + \frac{2\sqrt{7}}{2(3 + \sqrt{7})} \cos \theta + \frac{5}{2(3 + \sqrt{7})} \cos^2 \theta$$

■

9.9

Show that the directivity pattern of the third-order hypercardioid can be expressed as

$$B_{3,Hd}(\cos \theta) = -\frac{3}{32} - \frac{15}{32} \cos \theta + \frac{15}{32} \cos^2 \theta + \frac{35}{32} \cos^3 \theta.$$

Solution:

We know the definition of B:

$$B_{N,Hd}(\cos \theta) = \frac{1^T H^{-1}_N p(\cos \theta)}{1^T H^{-1}_N 1}$$

and for N=3:

$$\begin{aligned} p(\cos \theta) &= [1 \ cos \theta \ cos^2 \theta \ cos^3 \theta]^T \\ 1^T &= [1 \ 1 \ 1 \ 1] \end{aligned}$$

$$1 = [1 \ 1 \ 1 \ 1]^T$$

$$H_1 = \begin{pmatrix} 1 & 0 & \frac{1}{3} & 0 \\ 0 & \frac{1}{3} & 0 & \frac{1}{5} \\ \frac{1}{3} & 0 & \frac{1}{5} & 0 \\ 0 & \frac{1}{5} & 0 & \frac{1}{7} \end{pmatrix} \rightarrow H_1^{-1} = \begin{pmatrix} \frac{9}{4} & 0 & \frac{-15}{4} & 0 \\ 0 & \frac{75}{4} & 0 & \frac{-105}{4} \\ -\frac{15}{4} & 0 & \frac{45}{4} & 0 \\ 0 & -\frac{105}{4} & 0 & \frac{175}{4} \end{pmatrix}$$

substituting:

$$B_{3,Hd} = \frac{[1 \ 1 \ 1 \ 1] \begin{pmatrix} \frac{9}{4} & 0 & \frac{-15}{4} & 0 \\ 0 & \frac{75}{4} & 0 & \frac{-105}{4} \\ -\frac{15}{4} & 0 & \frac{45}{4} & 0 \\ 0 & -\frac{105}{4} & 0 & \frac{175}{4} \end{pmatrix} [1 \ \cos \theta \ \cos^2 \theta \ \cos^3 \theta]^T}{[1 \ 1 \ 1 \ 1] \begin{pmatrix} \frac{9}{4} & 0 & \frac{-15}{4} & 0 \\ 0 & \frac{75}{4} & 0 & \frac{-105}{4} \\ -\frac{15}{4} & 0 & \frac{45}{4} & 0 \\ 0 & -\frac{105}{4} & 0 & \frac{175}{4} \end{pmatrix} [1 \ 1 \ 1 \ 1]^T} =$$

$$= \frac{-\frac{3}{2} - \frac{15}{2} \cos \theta + \frac{15}{2} \cos^2 \theta + \frac{35}{2} \cos^3 \theta}{16} = -\frac{3}{32} - \frac{15}{32} \cos \theta + \frac{15}{32} \cos^2 \theta + \frac{35}{32} \cos^3 \theta$$

■

9.11

Show that the beampattern, the DF, and the WNG of the first-order DSA can be approximated as

$$\mathcal{B}[\mathbf{h}_1(f), \cos \theta] \approx \frac{1}{1 - \alpha_{1,1}} \cos \theta - \frac{\alpha_{1,1}}{1 - \alpha_{1,1}},$$

$$\mathcal{D}[\mathbf{h}_1(f)] \approx \frac{(1 - \alpha_{1,1})^2}{\alpha_{1,1}^2 + \frac{1}{3}},$$

$$\mathcal{W}[\mathbf{h}_1(f)] \approx \frac{1}{2} [2\pi f \tau_0 (1 - \alpha_{1,1})]^2.$$

Solution:

First we know that the beampattern is:

$$B[h_1(f), \cos \theta] = \frac{1 - e^{j2\pi f \tau_0 (\cos \theta - \alpha_{1,1})}}{1 - e^{j2\pi f \tau_0 (1 - \alpha_{1,1})}}$$

using the approximation:

$$e^x \approx 1 + x$$

we can approximate the beampattern as:

$$B[h_1(f), \cos \theta] = \frac{1 - e^{j2\pi f \tau_0 (\cos \theta - \alpha_{1,1})}}{1 - e^{j2\pi f \tau_0 (1 - \alpha_{1,1})}} \approx \frac{1 - 1 - j2\pi f \tau_0 (\cos \theta - \alpha_{1,1})}{1 - 1 - j2\pi f \tau_0 (1 - \alpha_{1,1})} = \frac{1}{1 - \alpha_{1,1}} \cos \theta - \frac{\alpha_{1,1}}{1 - \alpha_{1,1}}$$

■

we know that the DF is:

$$D[h_1(f)] = \frac{1 - \cos[2\pi f \tau_0 (1 - \alpha_{1,1})]}{1 - \sin c(2\pi f \tau_0) \cos(2\pi f \tau_0 \alpha_{1,1})}$$

Using the approximations:

$$\cos x \approx 1 - \frac{x^2}{2}$$

$$\sin cx \approx 1 - \frac{x^2}{6}$$

the DF becomes:

$$D[h_1(f)] \approx \frac{1 - 1 + \frac{[2\pi f \tau_0 (1 - \alpha_{1,1})]^2}{2}}{1 - \left(1 - \frac{(2\pi f \tau_0)^2}{6}\right) \left(1 - \frac{(2\pi f \tau_0 \alpha_{1,1})^2}{2}\right)} = \frac{\frac{[2\pi f \tau_0 (1 - \alpha_{1,1})]^2}{2}}{1 - \left(1 - \frac{(2\pi f \tau_0)^2}{6} - \frac{(2\pi f \tau_0 \alpha_{1,1})^2}{2} + \frac{(2\pi f \tau_0)^4 \alpha_{1,1}^2}{12}\right)}$$

$$\approx \frac{\frac{[2\pi f \tau_0(1-\alpha_{1,1})]^2}{2}}{\frac{(2\pi f \tau_0)^2}{6} + \frac{(2\pi f \tau_0 \alpha_{1,1})^2}{2}} = \frac{(1-\alpha_{1,1})^2}{\frac{1}{3} + \alpha_{1,1}^2}$$

■

The WNG is:

$$W[h_1(f)] = \frac{1}{2} \left| 1 - e^{j2\pi f \tau_0(1-\alpha_{1,1})} \right|^2 = 1 - \cos[2\pi f \tau_0(1 - \alpha_{1,1})]$$

using the cos approximation:

$$W[h_1(f)] \approx 1 - 1 + \frac{[2\pi f \tau_0(1 - \alpha_{1,1})]^2}{2} = \frac{1}{2}[2\pi f \tau_0(1 - \alpha_{1,1})]$$

■

9.12

Show that the inverse of the Vandermonde matrix $\mathbf{V}(f)$ that appears in (??) is given by

$$\mathbf{V}^{-1}(f) = \begin{bmatrix} v_2 v_3 & v_1 v_3 & v_1 v_2 \\ \frac{(v_2 - v_1)(v_3 - v_1)}{v_2 + v_3} & \frac{(v_2 - v_1)(v_3 - v_2)}{v_1 + v_3} & \frac{(v_3 - v_1)(v_3 - v_2)}{v_1 + v_2} \\ \frac{(v_2 - v_1)(v_3 - v_1)}{1} & \frac{(v_2 - v_1)(v_3 - v_2)}{1} & \frac{(v_3 - v_1)(v_3 - v_2)}{1} \\ \frac{(v_2 - v_1)(v_3 - v_1)}{(v_2 - v_1)(v_3 - v_1)} & \frac{(v_2 - v_1)(v_3 - v_2)}{(v_2 - v_1)(v_3 - v_2)} & \frac{(v_3 - v_1)(v_3 - v_2)}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix}.$$

Solution:

The inverse of the Vandermonde matrix is given by:

$$V^{-1}(f) = U(f)L(f)$$

where,

$$U(f) = \begin{bmatrix} 1 & -v_1 & v_1 v_2 \\ 0 & 1 & -(v_1 + v_2) \\ 0 & 0 & 1 \end{bmatrix}$$

$$L(f) = \begin{bmatrix} 1 & 0 & 0 \\ \frac{1}{v_1 - v_2} & \frac{1}{v_2 - v_1} & 0 \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{(v_2 - v_1)(v_2 - v_3)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix}$$

substituting U L in order to find the inverse of the Vandermonde matrix :

$$V^{-1}(f) = \begin{bmatrix} 1 & -v_1 & v_1 v_2 \\ 0 & 1 & -(v_1 + v_2) \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ \frac{1}{v_1 - v_2} & \frac{1}{v_2 - v_1} & 0 \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{(v_2 - v_1)(v_2 - v_3)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix} =$$

$$= \begin{bmatrix} 1 - \frac{v_1}{v_1 - v_2} + \frac{v_1 v_2}{(v_1 - v_2)(v_1 - v_3)} & -\frac{v_1}{v_2 - v_1} + \frac{v_1 v_2}{(v_2 - v_1)(v_2 - v_3)} & \frac{v_1 v_2}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{1}{v_1 - v_2} - \frac{v_1 + v_2}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{v_2 - v_1} - \frac{v_1 + v_2}{(v_2 - v_1)(v_2 - v_3)} & \frac{-(v_1 + v_2)}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{(v_2 - v_1)(v_2 - v_3)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix} =$$

$$= \begin{bmatrix} \frac{(v_1 - v_2)(v_1 - v_3) - v_1(v_1 - v_3) + v_1 v_2}{(v_1 - v_2)(v_1 - v_3)} & \frac{-v_1(v_2 - v_3) + v_1 v_2}{(v_2 - v_1)(v_2 - v_3)} & \frac{v_1 v_2}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{(v_1 - v_3)(v_1 + v_2)}{(v_1 - v_2)(v_1 - v_3)} & \frac{(v_2 - v_3)(v_1 + v_2)}{(v_2 - v_1)(v_2 - v_3)} & \frac{-(v_1 + v_2)}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{(v_2 - v_1)(v_2 - v_3)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix} =$$

$$= \begin{bmatrix} \frac{v_1 v_1 - v_1 v_3 - v_2 v_1 + v_2 v_3 - v_1 v_1 + v_1 v_3 + v_1 v_2}{(v_1 - v_2)(v_1 - v_3)} & \frac{-v_1 v_2 + v_1 v_3 + v_1 v_2}{(v_2 - v_1)(v_2 - v_3)} & \frac{v_1 v_2}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{v_1 - v_3 - v_1 - v_2}{(v_1 - v_2)(v_1 - v_3)} & \frac{v_2 - v_3 - v_1 - v_2}{(v_2 - v_1)(v_2 - v_3)} & \frac{-(v_1 + v_2)}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \frac{1}{(v_2 - v_1)(v_2 - v_3)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix} =$$

$$= \begin{bmatrix} \frac{v_2 v_3}{(v_2 - v_1)(v_3 - v_1)} & \frac{-v_1 v_3}{(v_2 - v_1)(v_3 - v_2)} & \frac{v_1 v_2}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{-(v_3 + v_2)}{(v_2 - v_1)(v_3 - v_1)} & \frac{v_1 + v_3}{(v_2 - v_1)(v_3 - v_2)} & \frac{-(v_1 + v_2)}{(v_3 - v_1)(v_3 - v_2)} \\ \frac{1}{(v_2 - v_1)(v_3 - v_1)} & \frac{-1}{(v_2 - v_1)(v_3 - v_2)} & \frac{1}{(v_3 - v_1)(v_3 - v_2)} \end{bmatrix}$$

■

9.13

Show that in the case of a second-order DSA with a zero of multiplicity 2 in the beampattern, the beamformer is given by

$$\mathbf{h}_{2,0}(f) = \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{2,1})}]^2} \begin{bmatrix} 1 \\ -2e^{-j2\pi f\tau_0\alpha_{2,1}} \\ e^{-j4\pi f\tau_0\alpha_{2,1}} \end{bmatrix},$$

we want to solve the following linear problem:

$$\begin{bmatrix} d^H(f, 1) \\ d^H(f, \alpha_{2,1}) \\ \sum d(f, \alpha_{2,1})^H \end{bmatrix} h(f) = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

$$\rightarrow \begin{bmatrix} 1 & v_1 & v_1^2 \\ 1 & v_2 & v_2^2 \\ \sum d(f, \alpha_{2,1})^H \end{bmatrix} h(f) = \begin{bmatrix} 1 & e^{j2\pi f\tau_0} & e^{j4\pi f\tau_0} \\ 1 & e^{j2\pi f\tau_0\alpha_{2,1}} & e^{j4\pi f\tau_0\alpha_{2,1}} \\ \sum d(f, \alpha_{2,1})^H \end{bmatrix} h(f) = \begin{bmatrix} [1 & e^{j2\pi f\tau_0} & e^{j4\pi f\tau_0}] h(f) \\ [1 & e^{j2\pi f\tau_0\alpha_{2,1}} & e^{j4\pi f\tau_0\alpha_{2,1}}] h(f) \\ \sum d(f, \alpha_{2,1})^H h(f) \end{bmatrix} = \otimes$$

using that $\sum d(f, \alpha_{2,1})^H h(f) = 0$:

$$\rightarrow \otimes = \begin{bmatrix} [1 & e^{j2\pi f\tau_0} & e^{j4\pi f\tau_0}] h(f) \\ [1 & e^{j2\pi f\tau_0\alpha_{2,1}} & e^{j4\pi f\tau_0\alpha_{2,1}}] h(f) \\ 0 \end{bmatrix}$$

and finally its easy to see that the solution $h(f)$ is:

$$h_{2,0}(f) = \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{2,1})}]^2} \begin{bmatrix} 1 \\ -2e^{-j2\pi f\tau_0\alpha_{2,1}} \\ e^{-j4\pi f\tau_0\alpha_{2,1}} \end{bmatrix}$$

■

the beampattern can be written as

$$\mathcal{B}[\mathbf{h}_{2,0}(f), \cos \theta] \approx \frac{1}{(1 - \alpha_{2,1})^2} (\cos \theta - \alpha_{2,1})^2,$$

Solution:

the beampattern has the form:

$$B[h_{2,0}(f), \cos \theta] = \frac{[1 - e^{j2\pi f\tau_0(\cos \theta - \alpha_{2,1})}]^2}{[1 - e^{j2\pi f\tau_0(1 - \alpha_{2,1})}]^2}$$

using the following approximation:

$$e^x \approx 1 + x$$

we get:

$$B[h_{2,0}(f), \cos \theta] \approx \frac{[1 - 1 - j2\pi f\tau_0(\cos \theta - \alpha_{2,1})]^2}{[1 - 1 - j2\pi f\tau_0(1 - \alpha_{2,1})]^2} = \frac{[j2\pi f\tau_0(\cos \theta - \alpha_{2,1})]^2}{[j2\pi f\tau_0(1 - \alpha_{2,1})]^2} = \frac{[\cos \theta - \alpha_{2,1}]^2}{[1 - \alpha_{2,1}]^2}$$

■

The WNG can be approximated as

$$\mathcal{W}[\mathbf{h}_{2,0}(f)] \approx \frac{1}{6} [2\pi f\tau_0 (1 - \alpha_{2,1})]^4.$$

Solution:

We find that the WNG is:

$$W[h(f)] = \frac{1}{6} \left| 1 - e^{j2\pi f\tau_0(1-\alpha_{2,1})} \right|^4 = \frac{2}{3} [1 - \cos[2\pi f\tau_0(1 - \alpha_{2,1})]]^2$$

with the following approximation:

$$\cos x \approx 1 - \frac{x^2}{2}$$

The WNG can be approximated as

$$W[h(f)] \approx \frac{2}{3} \left[1 - 1 + \frac{[2\pi f \tau_0 (1 - \alpha_{2,1})]^2}{2} \right]^2 = \frac{2}{3 \cdot 4} [2\pi f \tau_0 (1 - \alpha_{2,1})]^4 = \frac{1}{6} [2\pi f \tau_0 (1 - \alpha_{2,1})]^4$$

■

9.14

Show that the first column of the inverse of the Vandermonde matrix $\mathbf{V}(f)$ that appears in (??) is given by

$$\mathbf{V}^{-1}(f; :, 1) = \begin{bmatrix} \frac{v_2 v_3 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \\ -\frac{v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \\ \frac{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)}{1} \\ -\frac{1}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \end{bmatrix}.$$

Solution:

The inverse of the Vandermonde matrix is given by:

$$V^{-1}(f) = U(f)L(f)$$

where,

$$U(f) = \begin{pmatrix} 1 & -v_1 & v_1 v_2 & -v_1 v_2 v_3 \\ 0 & 1 & -(v_1 + v_2) & v_1 v_2 + v_1 v_3 + v_3 v_2 \\ 0 & 0 & 1 & -(v_1 + v_2 + v_3) \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$L(f) = \begin{bmatrix} \frac{1}{1} & \dots \\ \frac{1}{(v_1 - v_2)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \end{bmatrix}$$

substituting U L in order to find the inverse of the Vandermonde matrix :

$$V^{-1}(f) = U(f)L(f) = \begin{pmatrix} 1 & -v_1 & v_1 v_2 & -v_1 v_2 v_3 \\ 0 & 1 & -(v_1 + v_2) & v_1 v_2 + v_1 v_3 + v_3 v_2 \\ 0 & 0 & 1 & -(v_1 + v_2 + v_3) \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{bmatrix} \frac{1}{1} & \dots \\ \frac{1}{(v_1 - v_2)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \end{bmatrix} =$$

$$= \begin{bmatrix} 1 + \frac{-v_1}{(v_1 - v_2)} + \frac{v_1 v_2}{(v_1 - v_2)(v_1 - v_3)} + \frac{-v_1 v_2 v_3}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ \frac{1}{(v_1 - v_2)} + \frac{-(v_1 + v_2)}{(v_1 - v_2)(v_1 - v_3)} + \frac{v_1 v_2 + v_1 v_3 + v_3 v_2}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)} + \frac{-(v_1 + v_2 + v_3)}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ 1 + \frac{1}{(v_1 - v_2)} + \frac{1}{(v_1 - v_2)(v_1 - v_3)} + \frac{1}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \end{bmatrix} = \begin{bmatrix} \frac{-v_2 v_3 v_4}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ \frac{v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ \frac{-v_2 - v_3 - v_4}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \\ \frac{1}{(v_1 - v_2)(v_1 - v_3)(v_1 - v_4)} & \dots \end{bmatrix} =$$

$$= \begin{bmatrix} \frac{v_2 v_3 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{-v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{v_2 + v_3 + v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{-1}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \end{bmatrix}$$

so we get:

$$V^{-1}(f) = \begin{bmatrix} \frac{v_2 v_3 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{v_2 + v_3 + v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \\ \frac{1}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} & \dots \end{bmatrix}$$

■

9.15

Show that the third-order DSA beamformer is given by

$$\mathbf{h}_3(f) = \frac{1}{[1 - e^{j2\pi f \tau_0(1-\alpha_{3,1})}] [1 - e^{j2\pi f \tau_0(1-\alpha_{3,2})}] [1 - e^{j2\pi f \tau_0(1-\alpha_{3,3})}]} \times \\ \left[\begin{array}{c} 1 \\ -e^{-j2\pi f \tau_0 \alpha_{3,1}} - e^{-j2\pi f \tau_0 \alpha_{3,2}} - e^{-j2\pi f \tau_0 \alpha_{3,3}} \\ e^{-j2\pi f \tau_0 (\alpha_{3,1} + \alpha_{3,2})} + e^{-j2\pi f \tau_0 (\alpha_{3,2} + \alpha_{3,3})} + e^{-j2\pi f \tau_0 (\alpha_{3,1} + \alpha_{3,3})} \\ -e^{-j2\pi f \tau_0 (\alpha_{3,1} + \alpha_{3,2} + \alpha_{3,3})} \end{array} \right].$$

Solution:

first we know from (9.82):

$$V(f)h_3(f) = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$h_3(f) = V^{-1}(f) \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} = V^{-1}(f; :, 1)$$

as we know from problem 9.14 :

$$\rightarrow h_3(f) = \begin{bmatrix} \frac{v_2 v_3 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \\ -\frac{v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \\ \frac{v_2 + v_3 + v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \\ -\frac{1}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} \end{bmatrix}$$

Now let's simplify the phrase:

$$h_3(f, 1) = \frac{v_2 v_3 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} = \frac{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} = \\ = \frac{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} \frac{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}}{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}} \\ \rightarrow h_3(f, 1) = \frac{1}{(1 - e^{j2\pi f \tau_0(1-\alpha_{3,1})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,2})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,3})})}$$

$$h_3(f, 2) = -\frac{v_2 v_3 + v_3 v_4 + v_2 v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} = -\frac{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} + e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}} + e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} = \\ = -\frac{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} + e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}} + e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} \frac{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}}{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}} \\ \rightarrow h_3(f, 2) = -\frac{e^{-j2\pi f \tau_0 \alpha_{3,1}} + e^{-j2\pi f \tau_0 \alpha_{3,2}} + e^{-j2\pi f \tau_0 \alpha_{3,3}}}{(1 - e^{j2\pi f \tau_0(1-\alpha_{3,1})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,2})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,3})})}$$

$$h_3(f, 3) = \frac{v_2 + v_3 + v_4}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} = \frac{e^{j2\pi f \tau_0 \alpha_{3,1}} + e^{j2\pi f \tau_0 \alpha_{3,2}} + e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} = \\ = \frac{e^{j2\pi f \tau_0 \alpha_{3,1}} + e^{j2\pi f \tau_0 \alpha_{3,2}} + e^{j2\pi f \tau_0 \alpha_{3,3}}}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} \frac{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}}{\frac{1}{e^{j2\pi f \tau_0 \alpha_{3,1}} e^{j2\pi f \tau_0 \alpha_{3,2}} e^{j2\pi f \tau_0 \alpha_{3,3}}}} \\ \rightarrow h_3(f, 3) = \frac{e^{-j2\pi f \tau_0(\alpha_{3,1} + \alpha_{3,2})} + e^{-j2\pi f \tau_0(\alpha_{3,1} + \alpha_{3,3})} + e^{-j2\pi f \tau_0(\alpha_{3,2} + \alpha_{3,3})}}{(1 - e^{j2\pi f \tau_0(1-\alpha_{3,1})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,2})})(1 - e^{j2\pi f \tau_0(1-\alpha_{3,3})})}$$

$$h_3(f, 4) = -\frac{1}{(v_2 - v_1)(v_3 - v_1)(v_4 - v_1)} = -\frac{1}{(e^{j2\pi f \tau_0 \alpha_{3,1}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,2}} - e^{j2\pi f \tau_0})(e^{j2\pi f \tau_0 \alpha_{3,3}} - e^{j2\pi f \tau_0})} =$$

$$= -\frac{1}{(e^{j2\pi f\tau_0\alpha_{3,1}} - e^{j2\pi f\tau_0})(e^{j2\pi f\tau_0\alpha_{3,2}} - e^{j2\pi f\tau_0})(e^{j2\pi f\tau_0\alpha_{3,3}} - e^{j2\pi f\tau_0})} \frac{\frac{1}{e^{j2\pi f\tau_0\alpha_{3,1}} e^{j2\pi f\tau_0\alpha_{3,2}} e^{j2\pi f\tau_0\alpha_{3,3}}}}{\frac{1}{e^{j2\pi f\tau_0\alpha_{3,1}} e^{j2\pi f\tau_0\alpha_{3,2}} e^{j2\pi f\tau_0\alpha_{3,3}}}} \\ \rightarrow h_3(f, 4) = -\frac{e^{-j2\pi f\tau_0(\alpha_{3,1} + \alpha_{3,2} + \alpha_{3,3})}}{(1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1 - e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1 - e^{j2\pi f\tau_0(1-\alpha_{3,3})})}$$

and finally:

$$h_3(f) = \begin{bmatrix} \frac{1}{(1-e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,3})})} \\ \frac{e^{-j2\pi f\tau_0\alpha_{3,1}}+e^{-j2\pi f\tau_0\alpha_{3,2}}+e^{-j2\pi f\tau_0\alpha_{3,3}}}{(1-e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,3})})} \\ \frac{e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,2})}+e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,3})}+e^{-j2\pi f\tau_0(\alpha_{3,2}+\alpha_{3,3})}}{(1-e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,3})})} \\ \frac{e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,2}+\alpha_{3,3})}}{(1-e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1-e^{j2\pi f\tau_0(1-\alpha_{3,3})})} \end{bmatrix}$$

$$h_3(f) = \frac{1}{(1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})})(1 - e^{j2\pi f\tau_0(1-\alpha_{3,2})})(1 - e^{j2\pi f\tau_0(1-\alpha_{3,3})})} \begin{bmatrix} 1 \\ -e^{-j2\pi f\tau_0\alpha_{3,1}} - e^{-j2\pi f\tau_0\alpha_{3,2}} - e^{-j2\pi f\tau_0\alpha_{3,3}} \\ e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,2})} + e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,3})} + e^{-j2\pi f\tau_0(\alpha_{3,2}+\alpha_{3,3})} \\ -e^{-j2\pi f\tau_0(\alpha_{3,1}+\alpha_{3,2}+\alpha_{3,3})} \end{bmatrix}$$

■

9.16

Show that in the case of a third-order DSA with a zero of multiplicity 3 in the beampattern, the beamformer is given by

$$\mathbf{h}_{3,0}(f) = \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3} \begin{bmatrix} 1 \\ -3e^{-j2\pi f\tau_0\alpha_{3,1}} \\ 3e^{-j4\pi f\tau_0\alpha_{2,1}} \\ -e^{-j6\pi f\tau_0\alpha_{2,1}} \end{bmatrix},$$

Solution:

we want to solve the following linear problem:

$$\begin{bmatrix} d^H(f, 1) \\ d^H(f, \alpha_{3,1}) \\ \sum d^H(f, \alpha_{3,2})^H \\ \sum^2 d^H(f, \alpha_{3,3})^H \end{bmatrix} h(f)$$

so:

$$\begin{bmatrix} d^H(f, 1) \\ d^H(f, \alpha_{3,1}) \\ \sum d^H(f, \alpha_{3,2})^H \\ \sum^2 d^H(f, \alpha_{3,3})^H \end{bmatrix} h(f) = \begin{bmatrix} 1 & v_1 & v_1^2 & v_1^3 \\ 1 & v_2 & v_2^2 & v_2^3 \\ \sum d^H(f, \alpha_{3,2})^H \\ \sum^2 d^H(f, \alpha_{3,3})^H \end{bmatrix} h_{3,0}(f) = \begin{bmatrix} [1 & v_1 & v_1^2 & v_1^3] h_{3,0}(f) \\ [1 & v_2 & v_2^2 & v_2^3] h_{3,0}(f) \\ \sum d^H(f, \alpha_{3,2})^H h_{3,0}(f) \\ \sum^2 d^H(f, \alpha_{3,3})^H h_{3,0}(f) \end{bmatrix} = (a)$$

from 9.86 we know:

$$(j2\pi f\tau_0) \sum d^H(f, \alpha_{3,2})^H h_{3,0}(f) = 0 \rightarrow \sum d^H(f, \alpha_{3,2})^H h_{3,0}(f) = 0$$

and from 9.87 we know:

$$(j2\pi f\tau_0)^2 \sum^2 d^H(f, \alpha_{3,3})^H h_{3,0}(f) = 0 \rightarrow \sum^2 d^H(f, \alpha_{3,3})^H h_{3,0}(f) = 0$$

substituting:

$$(a) = \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3} \begin{bmatrix} 1 & e^{j2\pi f\tau_0} & e^{j4\pi f\tau_0} & e^{j6\pi f\tau_0} \\ 1 & e^{j2\pi f\tau_0\alpha_{3,1}} & e^{j4\pi f\tau_0\alpha_{3,1}} & e^{j6\pi f\tau_0\alpha_{3,1}} \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ -3e^{-j2\pi f\tau_0\alpha_{3,1}} \\ 3e^{-j4\pi f\tau_0\alpha_{3,1}} \\ -e^{-j6\pi f\tau_0\alpha_{3,1}} \end{bmatrix} =$$

$$\begin{aligned}
&= \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3} \begin{bmatrix} 1 - 3e^{-j2\pi f\tau_0\alpha_{3,1}}e^{j2\pi f\tau_0} + 3e^{-j4\pi f\tau_0\alpha_{3,1}}e^{j4\pi f\tau_0} - e^{-j6\pi f\tau_0\alpha_{3,1}}e^{j6\pi f\tau_0} \\ 1 - 3e^{-j2\pi f\tau_0\alpha_{3,1}}e^{j2\pi f\tau_0\alpha_{3,1}} + 3e^{-j4\pi f\tau_0\alpha_{3,1}}e^{j4\pi f\tau_0\alpha_{3,1}} - e^{-j6\pi f\tau_0\alpha_{3,1}}e^{j6\pi f\tau_0\alpha_{3,1}} \\ 0 \\ 0 \end{bmatrix} = \\
&= \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3} \begin{bmatrix} 1 - 3e^{j2\pi f\tau_0(1-\alpha_{3,1})} + 3e^{j4\pi f\tau_0(1-\alpha_{3,1})} - e^{j6\pi f\tau_0(1-\alpha_{3,1})} \\ 1 - 3 + 3 - 1 \\ 0 \\ 0 \end{bmatrix} = \\
&= \frac{1}{[1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3} \begin{bmatrix} [1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})}]^3 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}
\end{aligned}$$

■

the beampattern can be approximated as

$$\mathcal{B}[\mathbf{h}_{3,0}(f), \cos \theta] \approx \frac{1}{(1 - \alpha_{3,1})^3} (\cos \theta - \alpha_{3,1})^3,$$

Solution:

the beampattern has the form:

$$B[h_{3,0}(f), \cos \theta] = \frac{[1 - e^{j2\pi f\tau_0(\cos \theta - \alpha_{3,1})}]^3}{[1 - e^{j2\pi f\tau_0(1 - \alpha_{3,1})}]^3}$$

using the following approximation:

$$e^x \approx 1 + x$$

we get:

$$B[h_{3,0}(f), \cos \theta] \approx \frac{[1 - 1 - j2\pi f\tau_0(\cos \theta - \alpha_{3,1})]^3}{[1 - 1 - j2\pi f\tau_0(1 - \alpha_{3,1})]^3} = \frac{[j2\pi f\tau_0(\cos \theta - \alpha_{3,1})]^3}{[j2\pi f\tau_0(1 - \alpha_{3,1})]^3} = \frac{[\cos \theta - \alpha_{3,1}]^3}{[1 - \alpha_{3,1}]^3}$$

■

and the WNG can be approximated as

$$\mathcal{W}[\mathbf{h}_{3,0}(f)] \approx \frac{1}{20} [2\pi f\tau_0 (1 - \alpha_{3,1})]^6.$$

Solution:

We find that the WNG is:

$$W[h(f)] = \frac{1}{20} \left| 1 - e^{j2\pi f\tau_0(1-\alpha_{3,1})} \right|^6 = \frac{2}{5} [1 - \cos[2\pi f\tau_0(1 - \alpha_{3,1})]]^3$$

with the following approximation:

$$\cos x \approx 1 - \frac{x^2}{2}$$

The WNG can be approximated as

$$W[h(f)] \approx \frac{2}{5} \left[1 - 1 + \frac{[2\pi f\tau_0(1 - \alpha_{3,1})]^2}{2} \right]^3 = \frac{2}{5 \cdot 8} [2\pi f\tau_0(1 - \alpha_{3,1})]^6 = \frac{1}{20} [2\pi f\tau_0(1 - \alpha_{3,1})]^6$$

■

9.18

Show that the beampattern, the WNG, and the DF of the minimum-norm beamformer are given by

$$\begin{aligned}\mathcal{B}[\mathbf{h}_{MN}(f, \alpha, \beta), \cos \theta] &= \mathbf{d}^H(f, \cos \theta) \mathbf{D}^H(f, \alpha) \times \\ &\quad [\mathbf{D}(f, \alpha) \mathbf{D}^H(f, \alpha)]^{-1} \beta, \\ \mathcal{W}[\mathbf{h}_{MN}(f, \alpha, \beta)] &= \frac{1}{\beta^T [\mathbf{D}(f, \alpha) \mathbf{D}^H(f, \alpha)]^{-1} \beta}, \\ \mathcal{D}[\mathbf{h}_{MN}(f, \alpha, \beta)] &= \frac{1}{\mathbf{h}_{MN}^H(f, \alpha, \beta) \Gamma_{0,\pi}(f) \mathbf{h}_{MN}(f, \alpha, \beta)}.\end{aligned}$$

Solution:

First we know:

$$\begin{aligned}(1) h_{MN}(f, \alpha, \beta) &= D^H(f, \alpha) [D(f, \alpha) D^H(f, \alpha)]^{-1} \beta \\ (2) h_{MN}(f, \alpha, \beta)^H d(f, 1) &= 1\end{aligned}$$

It is easy to see that the beampattern is:

$$\begin{aligned}B[h_{MN}(f, \alpha, \beta), \cos \theta] &= d^H(f, \cos \theta) h_{MN}(f, \alpha, \beta) = \\ &= d^H(f, \cos \theta) D^H(f, \alpha) [D(f, \alpha) D^H(f, \alpha)]^{-1} \beta\end{aligned}$$

■

The WNG defined as:

$$W[h(f)] = \frac{|h^H(f)d(f, 1)|^2}{h^H(f)h(f)}$$

substitute (1) and (2) to the definition of WNG:

$$\begin{aligned}W[h_{MN}(f)] &= \frac{|h_{MN}^H(f, \alpha, \beta)d(f, 1)|^2}{h_{MN}^H(f, \alpha, \beta)h_{MN}(f, \alpha, \beta)} = \\ &= \frac{1^2}{\beta^H(f, \alpha) [D(f, \alpha) D^H(f, \alpha)]^{-1} [D(f, \alpha) D^H(f, \alpha)] [D(f, \alpha) D^H(f, \alpha)]^{-1} \beta} = \\ &= \frac{1}{\beta^H(f, \alpha) [D(f, \alpha) D^H(f, \alpha)]^{-1} \beta}\end{aligned}$$

■

The DF of the minimum-norm beamformer defined as:

$$D[h(f)] = \frac{|h^H(f)d(f, 1)|^2}{h^H(f)\Gamma_{0,2\pi}h(f)}$$

substitute (1) and (2) to the definition of the DF;

$$D[h_{MN}(f, \alpha, \beta)] = \frac{|h_{MN}^H(f, \alpha, \beta)d(f, 1)|^2}{h_{MN}^H(f, \alpha, \beta)\Gamma_{0,2\pi}h_{MN}(f, \alpha, \beta)} = \frac{1}{h_{MN}^H(f, \alpha, \beta)\Gamma_{0,2\pi}h_{MN}(f, \alpha, \beta)}$$